Assessment of the protective function of forests against debris flows in a gorge of the Slovenian Alps

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Protection forests play an important role in mitigating the influence of natural hazards. Despite the growing need for protective functions due to aging forests and increased risk of natural disturbances, active forest management has become increasingly uncommon across the Alps. Active management of protection forests can be facilitated by state subsidies. This requires an objective delineation of forests with a direct protection function and the development of silvicultural techniques that mitigate natural hazards. A study of protection efficiency of beech-dominated forests was performed in the Soteska gorge in NW Slovenia, where a main state road and railway are at risk from debris flows and rockfall. We assessed the starting points of debris-flow hazard based on a small-scale geological survey of the terrain characteristics and a local debris flow susceptibility map. We applied the TopRunDF model for determination of the run-out zones. Forest structure data were obtained from 26 sample plots. A detailed description and delineation of forest stands was performed. The results showed that these forests play an important role in the protection of infrastructure. Forest protection efficiency can be improved by stand thinning for stability and careful planning of regeneration patches over time and space. In areas where silvicultural measures cannot provide sufficient protection, technical measures are needed. Since these forests have not been managed for several decades, natural disturbances (windthrow) are frequent. Research findings suggest that regular assessment and management of these beech-dominated protection forests are necessary, contrary to the current practice of non-management in protection forests in Slovenia.

Keywords: Protection Forest, Protection Function, Debris Flow, TopRunDF, Beech Forest

Introduction

Traditional land use (agriculture and forestry) is being abandoned in the Alps due to socioeconomic changes, while an increasingly larger area is being used for tourism and infrastructure, which requires protection from natural hazards. Forests provide permanent protective functions, but only if they are properly and sustainably managed (Ott et al. 1997, O’Hara 2006, Mizunaga et al. 2010). There has been a general decline in forest management in Europe (Forest Europe 2010) and in the Alps in particular, where it is difficult to achieve positive economic returns (Schütz 1996). Climate change has increased the frequency of extraordinary weather phenomena, which causes higher risk from natural hazards and weakening of forest stability (Seidl et al. 2011). In many Alpine countries, state subsidies are used to facilitate the management of forests with direct protective functions (Mayer & Ott 1991, Brang et al. 2006). In order to maximize protective effects with minimal costs, a thorough understanding of natural hazards, their impact areas, and the potential role of forests is necessary (Lopez Saez et al. 2011). A detailed delineation of forest areas with direct protective functions is necessary to determine the areas where state subsidies should be directed. In addition, forest profile models must be developed to inform silvicultural measures and to verify their success (Mayer & Ott 1991, Berger & Rey 2004, Frehner et al. 2005).

In Switzerland a method for the delineation of forests with direct protection functions was developed as part of the Silvaprotection project: a standardized delineation of protection forests at the state level. The procedure involves multiple, stepwise modules that generate the actual forest areas with direct protection functions (Giamboni & Wehrli 2008). In France, the zoning classification of mountain forests with direct protection functions and the mapping of hazards and prohibition of the construction of infrastructure in risk areas were identified as the most effective preventive approach to ensure the maintenance of protective functions (Berger & Rey 2004). In Austria, a distinction is made between two types of protection forests: site-protection forests and infrastructure-protection forests, the latter also including forests that protect against noise and light pollution (Schima & Singer 2008). Delineation methods of forests in which slope processes (e.g., erosion, landslides, debris flow, etc.) are present differ among the federal states (Ziegner 2002).

The negative effects of disturbances are best mitigated by uneven aged forests, where the presence and distribution of trees provide protection against natural hazards, and the ability to replace damaged trees with existing regeneration provides elasticity (O’Hara 2006). For such forests it is necessary to determine a (modified) selection forest target profile. In Switzerland the NaPh - Nachhaltigkeit und Erfolgskontrolle im Schutzwald is used for the management of protection forests (Frehner et al. 2005). The method is used to assess a protection forest by comparing the current state of a stand with the target profile for each site and natural hazard (Brang et al. 2006). Motta & Hauenschild (2000) evaluated protection forests in a similar way in Italy.

Despite extensive research and development projects on Alpine forests and protective functions (Ott et al. 1997, Brang et al. 2006), there are relatively few studies of beechnut protection forests, even though beech forests are the potential natural vegetation of nearly the entire boundary of the Alpine range. There are even fewer studies of beech protection forests in southeastern Europe, where beech is the dominant tree species. Beech is a species with several specific cha-
characteristics: seeds are produced unevenly and only occasionally in abundance (Korpel 1995); the plasticity of beech canopies (lateral growth) quickly closes canopy gaps, re-
straining the growth of regeneration (Ellen-
borg 1996). Precipitation and evaporation is in gaps and un-
der closed canopy. Beech forests have a na-
tural tendency towards vertically even struc-
tured composition (Leibundgut 1982, Otto 1994). Beech is a shade tolerant species, but does not tolerate long-term, almost complete canopy closure, particularly under its own closed canopy (Meyer et al. 2003). Addi-
tionally, the asymmetry of beech crowns, es-
specially noticeable on slopes, makes it difficult to execute felling in the desired direction and to protect advance regeneration. Maintaining a sustainable selection structure is, therefore, more difficult in beech forests. In general, the selection management of pure beech re-
quires slightly lower growing stock and mo-
re frequent interventions than mixed beech selec-
tion systems (Schütz 2001a). Forest ve-
gestation has a major effect on the stability of slopes by influencing hydrological processes (which affect water content in the soil and the pore pressure) and soil mechanical struc-
ture (which affects soil strength). The latter is performed by two root actions. Firstly, small flexible roots mobilize their tensile strength by root-soil friction and thereby in-
crease the compound matrix (soil-fibre) strength. Secondly, large roots intercept the shear surface and act as individual anchors that eventually slip through the soil without braking, thereby mobilizing a soil-root fric-
tion force instead of the entire tensile strength (Bischetti et al. 2005, 2009).

As a type of mass movement of sediments on slopes or torrent channels, debris flows have reconfigured the terrain of Slovenia and their frequency has been increasing. Disper-
sed settlement and the dense network of transport routes require a detailed study of hazards that debris flows pose to the envi-
ronment (Sodnik & Mikoš 2006, Lopez Saez et al. 2011). Furthermore, Slovenia does not yet have a much-needed legal basis for pre-
ventive protection from increasingly fre-
cquent debris flows (Cetina et al. 2006, Mi-
koš et al. 2004, Mikoš et al. 2006). Collab-
oration among disciplines such as forestry, hydrology, and geology is required for the identification of the location and the deter-
mination of impact areas of phenomena such as erosion, debris flows, and landslides.

NW Slovenia has frequent intensive down-
pours and high precipitation compared to the rest of the Alps (Frei 1995). Days with 100 mm of precipitation are not infrequent and the highest daily precipitation in Slovenia has been recorded in nearby Bohinj where over 400 mm of rain fell in 24 hours (Kajčič-
Bošnjak 1986). High precipitation is a condi-
tion for the occurrence of debris flows on geomorphologically heterogeneous, erodible

topography, such as the Soteska study area. In the broader region, beech forms natural stands that range from the lowlands up to the upper timberline (1800-2000 m a.s.l.). Stands in Soteska have been ageing due to lack of management. In the transition from the optimal phase to the regeneration phase, a stand breaks down, resulting in reduction of its protection function (Motta & Haude-
mund 2000). The degree of stand breakdown is also determined by disturbances in forest ecosystems (Picket & White 1985). Rock-
falls, avalanches as well as windthrow events drive stand development. If their magnitudes are sufficiently small, they exert a positive impact on the regeneration dynamics of fo-
rest stands (Dorren & Berger 2006), but at greater magnitudes or in more sensitive fo-
rests, they can completely interrupt the pro-
tective functions of a forest for decades (Mayer & Ott 1991). Given the geomorpho-
logical characteristics of the site, the history of non-management, and the infrastructure present downslope, the forests in Soteska are an ideal case study for the methodology of delineation of forests with direct protection function, and for the development of plan-
ing tools for the management of protection forests.

Our objectives were to: (i) carry out spa-
tially-explicit modeling to identify areas where debris flows may occur; (ii) assess the protective effect of forest stands against de-
bris flows; (iii) compare the actual state of the structural characteristics of the forest with a target profile; and (iv) analyse the fea-
sibility and suitability of silvicultural mea-
sures.

Materials and methods

Study area

The Soteska gorge is a narrow alpine valley along the Sava Bohinjka River (NW Slove-
nia) that drains the Bohinj Lake, and, toge-
 ther with the Sava Dolinka River, forms the Sava River (the largest and longest river in Slovenia). The study area consists of 207 ha of protection forests in which regular cutting is restricted according to the 1993 Forest Act (Official Gazette 1993). Altitudes range from about 470 m a.s.l. (Sava Bohinjka River) up to 1200 m a.s.l. The slopes are very steep (mean slope angle of 35°) and include nume-
rous cliff faces. The coarse-scale topography is very heterogeneous and is characterized by highly dissected slopes and abundant rock outcrops and cliffs. The slopes on the right bank of the river are dominated by northern, northwestern, and western exposi-
tions. Stoniness and rockiness are present on almost all plots, indicating relatively shallow soils. Old scree are mostly overgrown with forest, though there are individual exposed scree sections with little soil. The dominant soil type is moderately deep to shallow, strongly skeletal moder rendzinas, which have a dense interconnected root system and are heavily water-logged, humus-rich, not very acidic, and immediately to well-sup-
plied with nutrients (FMP 2003). Soteska is characterized by a cool and humid climate, with abundant precipitation. The number of days with precipitation of at least 1 mm in this part of Slovenia is over 140 (ARSO 2006). Average annual precipitation at the nearest meteorological station (Stara Fužina, 547 m a.s.l., 1971-2000) is 2250 mm. Aver-
age temperature is -2.0 °C in the coldest month (January) and 17.6 °C in the warmest (July). Average annual temperature is 7.9 °C. Debris flows are created by a sufficient quantity of torrential water, which collects due to the damming of surface water or, more frequently, due to strong local precipi-
tation (Wiecezrek & Glade 2005). The do-
minant association in this environment is Anemone trifoliae-Fagetum, which grows at 600-1200 m a.s.l. on predominantly steep slopes on all exposures. It is a zonal associa-
tion of the Alpine phytogeographical area of the Illyrian floral province. European beech (Fagus sylvatica L.) forests have a stable bioecenotic structure (Marinček & Carni 2002). European beech populates the slopes of Soteska from the bottom to the edge of the plateau, occasionally transitioning to mixed silver fir (Abies alba Mill.) beech fo-
rest sites, which dominate the mountain plateau above Soteska. On steep slopes and on canopies, Alpine beech forests transition to beech and European hop-hornbeam (Ostrya carpinifolia Scop.) or even to Euro-
pean hop-hornbeam and manna ash (Fraxi-
inus ornus L.) forests. Data on past manage-

Data collection

In 2010/2011 we established 26 circular permanent sample plots of 500 m² in size (12.62 m radius) on intersections of a 200 x 200 m grid on the slopes of the right bank of the Sava Bohinjka River. If a plot was obstruc-
ted by overhead power lines or if it was on inaccessible rocks or ditches, it was moved by 50 or 100 meters to ensure sufficient co-
verage of the studied forest. As part of the plot inventory we measured all living trees with diameter at breast height (DBH) ≥ 10 cm. We recorded tree species, azimuth, dis-
tance to plot center, and DBH. We used a SUUNTO compass, diameter tape, and Hag-
lof Vertex (model: Laser VL402).

We performed a detailed description of the forest stands, including species composition,
DF produces two estimates: (1) an inundated flow deposit phase on debris cones. TopRun dimension run-out simulation of the debris MCI = 50. The model is a tool for the two-dimensional run-out simulation of the debris flow. An increase in the MCI number indicates a significant expansion of the debris flow run-out zone (Scheidl 2009a). Based on testing, we used MCI = 50. 2. The start point of the simulation of the debris flow deposit (x,y). For the start points of the simulation we used: (2a) Apex of the cone, where the debris flow deposit phase begins; the start points were obtained from the geological map created by GSS. This method was used for the calculation of the actual deposits of the debris flows, thus creating a debris flow deposit map on the debris cone; (2b) erosion-prone sites upslope where the probability of debris flow start points is very high; the starting points were obtained from the debris-flow susceptibility map (Fig. 1). This method was used for the creation of a debris-flow warning map (Fig. 2). 3. Magnitude (volume) of debris flow in m$^3$. Torrent catchments were similar in size and relatively small. GSS estimated the magnitude according to the deposited material on the site from former debris events. Magnitude was set to 5000 m$^3$. 4. Mobility coefficient, which was determined through testing and was set to 50 (cones closer to the valley bottom) or 100 (cones upslope). The areas of simulated deposited material were compared with actual deposited material - we selected an MC number according to greatest overlying of simulated and actual deposit. All of the listed simulation parameters were used during the sensitivity analysis. Values of the individual simulation parame-

Fig. 1 - The debris-flow susceptibility map of the study area in the Sava Bohinjka River gorge Soteska.

The Geological Survey of Slovenia (GSS) created a geological map of the study area at a 1:5000 scale based on a field survey. A detailed geological map of the study area was created as an input for the debris flow susceptibility map of the Soteska gorge (Fig. 1). General lithological and structural geological data were taken into account in the creation of the geological map, with special emphasis on the identification of unconsolidated sediments such as scree deposits that can be involved in mass movement processes.

The debris flow susceptibility map was created with a methodology that the GSS developed for different spatial resolutions and different types of mass movements (e.g., landslide, mass-flow, rockfall). Such methodology is comprised of four consecutive phases that involve a synthesis of archived data, geostatistical modeling with the GSS algorithm (Komic 2005), elaboration of a geohazard map and field verification of the most susceptible areas. The mapping process was first tested in the municipality of Bovec, at a 1:25 000 scale (Bavec et al. 2005). In addition to data on lithology, crushed tectonic zones, and distance from structural elements, the impact analysis and creation of the susceptibility model included elevation data, slope and curvature, distance to surface waters, energy potential of streams, and 48-hour rainfall intensity. As a finished product, the model is transferable and compatible with all levels of warning and decision-making; it can be directly applied in the creation of spatial plans and is therefore an effective tool for the protection from geological hazards.

We modeled debris flows with the Top Run Debris Flow (TopRunDF) model, version 1.1. The model is a tool for the two-dimensional run-out simulation of the debris flow deposit phase on debris cones. TopRun DF produces two estimates: (1) an inundated simulation area combined with overflow probability of each related cell (this was used as Debris flow warning map - Fig. 2); and (2) a deposited area and the deposition height of each cell (not shown in the paper - Scheidl 2009a, 2009b). The goal is to identify areas of debris flow deposit hazard on a debris cone. The following input data were used for the simulation: a digital elevation model (we used a DEM with a resolution of 12.5 m obtained from the Surveying and Mapping Authority of the Republic of Slovenia) and the following simulation parameters:

1. The number of Monte Carlo iterations (MCI number) determines the lateral over-flow of the debris flow. An increase in the MCI number indicates a significant expansion of the debris flow run-out zone (Scheidl 2009a). Based on testing, we used MCI = 50.
2. The start point of the simulation of the debris flow deposit (x,y). For the start points of the simulation we used: (2a) Apex of the cone, where the debris flow deposit phase begins; the start points were obtained from the geological map created by GSS. This
Fieldwork observations. Within the impact areas we separately delineated the torrent channel with a buffer zone on the basis of the TM5 and the actual state; the surface areas of debris cones were obtained from the geological map made by GBS. The torrents and the fans define the area where silvicultural measures are not possible; structural measures were proposed for these areas.

Results

Forest structure

The slope angles on sample plots ranged from 15° to 50°. The average growing stock of all sample plots was 388 m³/ha (coefficient of variation (CV) = 45%). The average growing stock of the impact area was higher (405 m³/ha) than the average for the stratum “other” (382 m³/ha). The distribution of growing stock by 20 cm diameter classes was 24% in A, 53% in B, and 23% in the C class. The basal area was 30.9 m²/ha (CV = 40%). The upper height of the stand was 30 and 29 m for Norway spruce and beech, respectively. Beech was the dominant tree species in the total growing stock (64%), followed by Norway spruce (22%), European hop-hornbeam (4%), European larch (3%), and other tree species (whitebeam, Sorbus aria Cr.; silver fir; manna ash - 7%).

The cumulative frequency of trees by 5 cm diameter classes indicated a negative exponential distribution (NE) and suggested correspondence with a selection forest structure (Fig. 3). However, in small diameter classes, there was a high proportion of tree species that thrive on extreme sites: European hop-hornbeam, whitebeam, and manna ash. These species do not typically reach large diameters and heights. Moreover, the frequency of the dominant tree species, beech and Norway spruce, was not sufficient in smaller diameter classes (10 ≤ DBH ≤ 25 cm). This indicated that the stands were rather even sized, which is a typical feature of beech stands.

The diameter distribution for the joint sample of all the plots was classified as a variable form, whereas the second closest form was a negative exponential (q-ratio = 1.38 - Fig. 3). The results were similar when curves were fitted separately for the stratum impact area (q=1.34). However, tree frequency on extreme sites was lower and the discrepancy of the distribution compared to the negative exponential was higher, indicating bimodality with deficits in the 3rd, 4th, and 5th 5 cm diameter classes. In the stratum “other”, a negative exponential function with a small surplus of trees in diameter class 6 fitted the distribution of diameter classes best (q = 1.48). Divisions of the area into strata corresponded with the forest structure, as beech in the mature stage dominated the stratum impact area, while beech and European hop-
hornbeam forests and hop-hornbeam and manna ash forests, characterized by smaller-diameter trees, dominated the remaining area.

Regeneration densities were relatively low compared to managed forests (Tab. 1). For beech seedlings and saplings the CV of the frequency was 147 % and 167 %, respectively. The CV for Norway spruce seedlings and saplings was lower and amounted to 114 % and 95 %, respectively.

Debris-flow modeling

The debris flow source area map shows susceptibility to debris flows (Fig. 1). Cell size was 5 x 5 m. Coordinates from areas with very high susceptibility rate (areas where the probability of debris flows exceeds 57 %) were used as a starting points of debris flow in the TopRunDF model, thus creating the warning map.

The next result of the modeling was the debris flow warning map (Fig. 2), which is the first step in the protection process. The result is an inundated simulation area combined with the overflow possibility of each related cell. The map shows the maximum potential debris flow reach and is suitable to be used as a warning map.

NaiS stands and measures

The delineated debris flow impact area was 42 ha or 20 % of the total area (207 ha). Torrent channel and debris cones on which silvicultural management was not possible accounted for 16 ha or 40 % of the total impact area. On the remaining 60 % (26 ha) of the impact area silvicultural measures were necessary. Proportions of NaiS stands in the impact area (Fig. 2 and Fig. 4) and necessity of measures are as follows (Fig. 5):

- 10: 1.2 % (0.3 ha) - low necessity of measures (in the next 30-50 years);
- 11: 60.3 % (15.6 ha) - medium necessity of measures (in the next 10-30 years);
- 12: 3.1 % (0.8 ha) - high necessity of measures (in the next 0-10 years);
- 20: 35.4 % (8.8 ha) - low necessity of measures (in the next 30-50 years).

To create a silvicultural plan, we need spatially explicit data on forest stands with emphasis on debris flow protective functions (NaiS - Fig. 4) and elements of natural hazard. Forest protective functions and optimal

<table>
<thead>
<tr>
<th>Size class</th>
<th>Species</th>
<th>0.1m ≤ H &lt; 1.3m</th>
<th>1.3m ≤ H and DBH &lt; 10cm</th>
<th>Sum</th>
</tr>
</thead>
<tbody>
<tr>
<td>Beech</td>
<td>273</td>
<td>193</td>
<td>466</td>
<td></td>
</tr>
<tr>
<td>Spruce</td>
<td>489</td>
<td>129</td>
<td>618</td>
<td></td>
</tr>
<tr>
<td>Sum</td>
<td>762</td>
<td>322</td>
<td>1084</td>
<td></td>
</tr>
</tbody>
</table>

Tab. 1 - Frequency of regeneration of dominant species in the stand by size class (N/ha).
stand structures depend on stand location in the broader debris flow impact area. We divided the stands to source area and infiltration area stands. Combined with forest type (NaiS stands), this served as the basis for the proposed silvicultural measures. With aging stands and decreasing mechanical stability, management in the impact areas seems crucial for sustaining protection effects. For each type of forest (10, 11, 12, 20 - see above) a detailed silvicultural plan was defined. An example of planned silvicultural measures in a poorly regenerated beech stand with trees in just one NaiS diameter class (12) may look like this:

- **In the debris flow source area**: Preservation of woody vegetation. If the slope is not too steep, spatially explicit regeneration patches (0.06 ha in size) are formed; on regenerated areas the gaps should not exceed 0.12 ha. Oversized gaps on steep slopes encourage the development of grass, thus hindering regeneration development. Due to shallow soil and steep slopes, maintaining smaller-dimension trees is preferable. The density of trees with DBH ≤ 30 cm should be high, as a dense, interconnected root system keeps the soil together, reducing the possibility of landslides or erosion scars that can trigger debris flow. Coppicing is preferred. Large-dimension trees (DBH ≥ 40 cm) should be removed. Hop hornbeam and manna ash should be favored if present.

- **In the infiltration area**: Promotion of perpetual regeneration with small gaps. Regeneration is favored on areas of at least 200-500 m²/ha or on at least 3 % of the area. When regeneration reaches DBH 5-10 cm, the remaining upper story trees are removed. Smaller-diameter trees (DBH ≤ 40 cm) should dominate the stand structure. In order to achieve a small-scale, uneven-aged and uneven-sized structure (trees in at least 2 NaiS diameter classes), spatially explicit regeneration patches should be created.

**Discussion**

**Forest structure**

Single-tree selection maintains a suitable structure for protection forests, since small-scale, uneven-structured stands provide continuous protection (Ott et al. 1997, O’Hara 2006). A small-scale, uneven aged structure is also suitable for mimicking natural disturbances, as Alpine beech forests are characterized by frequent small-scale and intermediate-severity disturbances (Leibundgut 1982, Splechtna et al. 2005). If protection forests are managed, several balanced states can be achieved (Schütz 2001a). In the study area, the target profile of the selection forest should be adjusted to a forest protection function and debris-flow protection in particular. Target stands should constitute smaller-diameter trees (e.g., target DBH ≤ 40 cm), lower growing stock, higher frequency of trees in lower diameter classes, and denser regeneration (higher $q$ values of the negative exponential curve). The high proportion of beech and the specifics of skidding render it difficult to achieve a single-tree selection structure on the study area; group selection is more feasible. However, there is a significant discrepancy between the present stand condition and a balanced selection model of
the target profile. The interval of balanced growing stock for a mixed selection forest can be developed from the upper height of the stand multiplied by a factor of 10 or 11 (Diaci & Firm 2011). Considering the characteristics of beech growth in protection forests, the balanced growing stock is lower than that in mixed forests (Schütz 2001b), we used a factor of 9 or 10, which was also driven by our desire to achieve a forest structure adjusted to protective functions. In our example an upper height of 30 m produces an interval estimate for balanced growing stock of 270-300 m$^3$ ha$^{-1}$. The actual growing stock was, therefore, about 100 m$^3$ ha$^{-1}$ too high. Schütz (2001a) proposes an even lower growing stock (250 m$^3$ ha$^{-1}$) for more productive Langula-type beech selection forests. Given his assumptions, the basal area of the study area was about 10 m$^2$ ha$^{-1}$ too high. The same author reported the following distribution of growing stock by diameter class for a beech forest on southern expositions in the Swiss Jura (20-30 cm: 15 %; 35-50 cm: 34 %; over 55 cm: 51 %). Since European hop-hornbeam and other non-successional tree species accounted for a large proportion of growing stock in lower diameter classes in this study, the growing stock of this diameter class was suitable. The growing stock of the medium-diameter class was slightly too high. The upper diameter class accounted for a minor proportion of the total growing stock, which was appropriate since these are protection forests on steep slopes and shallow soil, where large-diameter trees have proven to be unstable.

In general, there was little regeneration in Soteska. Duc (1991) reported that in a selection forest (orig. Planterwald) the minimum required frequency of 50-130 cm height trees was between 310 and 830 ha$^{-1}$; Schütz (2001a) proposed 90-740 ha$^{-1}$ as the minimum. In the study area, we found 237 beech individuals and 489 spruce individuals, a total of 762 stems ha$^{-1}$ in the seedling class. The proposed minimum frequency of regeneration was not entirely comparable to this study, as we inventoried regeneration from 10 cm, knowing that the mortality of lower regeneration is higher. That considered, we deem the frequency of regeneration to be at the lower end of the minimum range for a selection forest. In the 0-8 cm diameter class, Schütz (2001a) proposed a minimum of 210-1460 individuals, while Duc (1991) proposed 257-1933 individuals in the 0.1-7.4 cm class. In the sapling class (130 cm height to DHI ≤ 10 cm) we counted 193 beech individuals and 129 spruce individuals, a total of 322 stems ha$^{-1}$. Trees in this class were very sparse in Soteska, which is also evident from Fig. 3 that shows only about 55 ha$^{-1}$ beech and spruce individuals in diameter class 3. Regeneration was present mostly in gaps, but we nevertheless recorded frequent small-scale regeneration-free gaps. Beech regenerated poorly on very rocky terrain, where spruce regenerated well. Where there is sufficient light, light demanding tree species (European hop-hornbeam, manna ash) dominate extreme terrain.

**Debris-flow modeling**

The sensitivity analysis of the TopRunDF simulation model showed that the mobility coefficient (MC) is the most significant factor for debris flow modeling. Specific relief (steep slope on debris flow run-out zones) sets Soteska clearly apart from the circumstances in which the empirical equation for the MC calculation was made. It turned out that at steeper torrent slopes, MC values change very little, indicating poor sensitivity of the empirical equation to higher slope angle values. This indicates that the empirical equation was developed in conditions with significantly shallower slopes, hence the distorted results for steeper slopes and more realistic results for shallower slopes. Overflow at higher mobility coefficients produced better and more likely results. For our study area it would be necessary to develop a different empirical equation based on past events (debris flows), or to modify the existing equation to adjust for torrents with steeper slopes. The problem with empirical models such as the TopRun DF model is that they are constrained by the conditions in which they were developed. In testing the impact of the number of Monte Carlo iterations, we found that the best results are produced when the value is 50. This was also established by Scheidl & Rickenmann (2009). Although modeling is typically the principal method for the creation of a hazard map, it is also appropriate for the creation of a warning map. The model has the following advantages: ease of use, speed of calculation (most simulations take only a few seconds), and rapid, simple, and undemanding acquisition of input data (parameters) for modeling. But it also has downsides: (i) Empiricism of the model. The model has its limitations, as it is based on the specific conditions in which it was created. The mobility coefficient turned out to be the biggest limitation. (ii) The necessary number of simulations to acquire probable results: probable results are achieved through a high number of simulations with a variety of parameter values. According to the rules for the classification of areas into risk classes (Official Gazette 2007), a warning map must include the boundary line of the potential reach of the event but not the probability of the event occurring. In our proposal for the creation of a warning map, we used modeling to show the maximum scale of potential debris flow events as well as the probability of occurrence (Fig. 2), which is a step forward from an ordinary warning map. Detailed mathematical modeling could also be used to create a hazard map, but TopRunDF does not handle this feature. This is because the rules determine guidelines for the classification of hazard classes, where debris-flow velocity is a criterion along with the debris-flow depth, but the model used in this study does not produce speed data. To determine accurate parameters of debris overflow it is necessary to use more complex mathematical models in which simulations are based on hydraulic equations (dynamic and continuity equation) and the debris-flow rheology must be taken into account (e.g., FLO-2D - O’Brien 2006).

In this study we used a 12.5 m resolution DEM for modeling; in the future we should, as a matter of necessity, include LiDAR images, which are very precise and have been widely used elsewhere (Lopez Saez et al. 2011).
In the remaining protection forests outside the debris flow impact areas, it is recommended to remove dead trees from torrent channels, establish a small-scale uneven-aged structure, and create spatially-explicit regeneration patches (small-scale regeneration patches of 200-500 m²). The portion of conifers should be preserved, in particular fir and larch; spruce is less suitable. Root tensile and root cohesion tests in Italian Alps show that beech roots are significantly more resistant and offer greater reinforcement of soil than spruce roots (Biscetti et al. 2005, 2009, Vergani et al. 2012). In addition, spruce is less suitable for these sites as compared to beech, due to its susceptibility to bark beetles, (three times) lower mechanical resistance to rockfall and weak compartmentalization of trunks after damage (Stokes et al. 2005).

Annual field surveys are required to monitor the state of the forest stands since factors considering protection forest are the most important criterion among other functions (Santopuoli et al. 2012).

Conclusions

Lower timber value makes beech forests and protection forests less interesting for management, particularly on steep slopes. Asymmetrical crowns and the large dimensions of trees make management more demanding and dangerous. Numerous protection forests in the Alps have therefore been largely unmanaged in recent decades; this is even more true for forests on massifs in southeastern Europe (Dinaric Alps, Carpathian Mountains). Protection forests undoubtedly need active management to sustain their protection role. To objectively delineate protection forests it is essential to define impact areas of all present natural hazards. This study uses modeling as an objective method for delineating protection forest with a debris flow hazard. Characteristics of a given forest in impact areas must be compared to characteristics defined in target profiles for specific site and natural hazard. Discrepancy between them leads us to create a detailed spatially explicit silvicultural plan which tends to maximize the protection function of the given stands. In protection forests, a selection structure is ideal since it mimics natural disturbances and ensures continuous protection. However, this approach renders it difficult to be applied because of a high proportion of beech and difficult skidding conditions that make logging activities economically less attractive. A more suitable approach would be a small scale group selection. Within forests in the debris flow source area, silvicultural measures tend to ensure maximal water use, preserve small-diameter and high density woody vegetation (which reinforce soils) and avoid large gap openings to prevent development of grasses and reducing possibility of landslides and erosion scars that can trigger debris flow. In the infiltration area, the goals of silvicultural measures are similar. Perpetual regeneration is favored across the whole area or distributed evenly in small gaps, thereby resulting in uneven-aged and uneven-sized structure. Smaller diameter trees (< 40 cm) are preferred, since larger trees have proven to be unstable on steep slopes. On torrents and areas where rocky debris prevails, mature trees are damaged and regeneration is absent. Forests on these areas do not play such a crucial role in mitigating debris flow overflow; therefore hydrotechnical measures (deflection dams, flexible net barriers, ground slacks, check dams, etc.) are needed.

In the future it is necessary to adopt regulations on debris flows, or amend the existing legislation. Geology and forestry professionals and hydraulic engineers need to become involved in creating a legal basis for the comprehensive treatment of risks to infrastructure by natural hazards and the assessment of the impact of forests: geologists with geological, avalanche, and debris flow susceptibility maps, etc.; hydraulic experts with their know-how of hydraulics (rheology) and hydrology; and forestry experts with silvicultural practices (long-term spatial and temporal dynamics) and the management of protection forests (evaluation of protective functions, adjusted inventories of protection forests). Researchers should be brought together in a European network to facilitate the improvement of knowledge on beech protection forests.

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